

# Evaluation of SWAT Auto-calibration using Diverse Efficiency Criteria

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## □ Introduction



Advances in  
Geosciences

# Comparison of different efficiency criteria for hydrological model assessment

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## SWAT model application

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### ARTICLE INFO

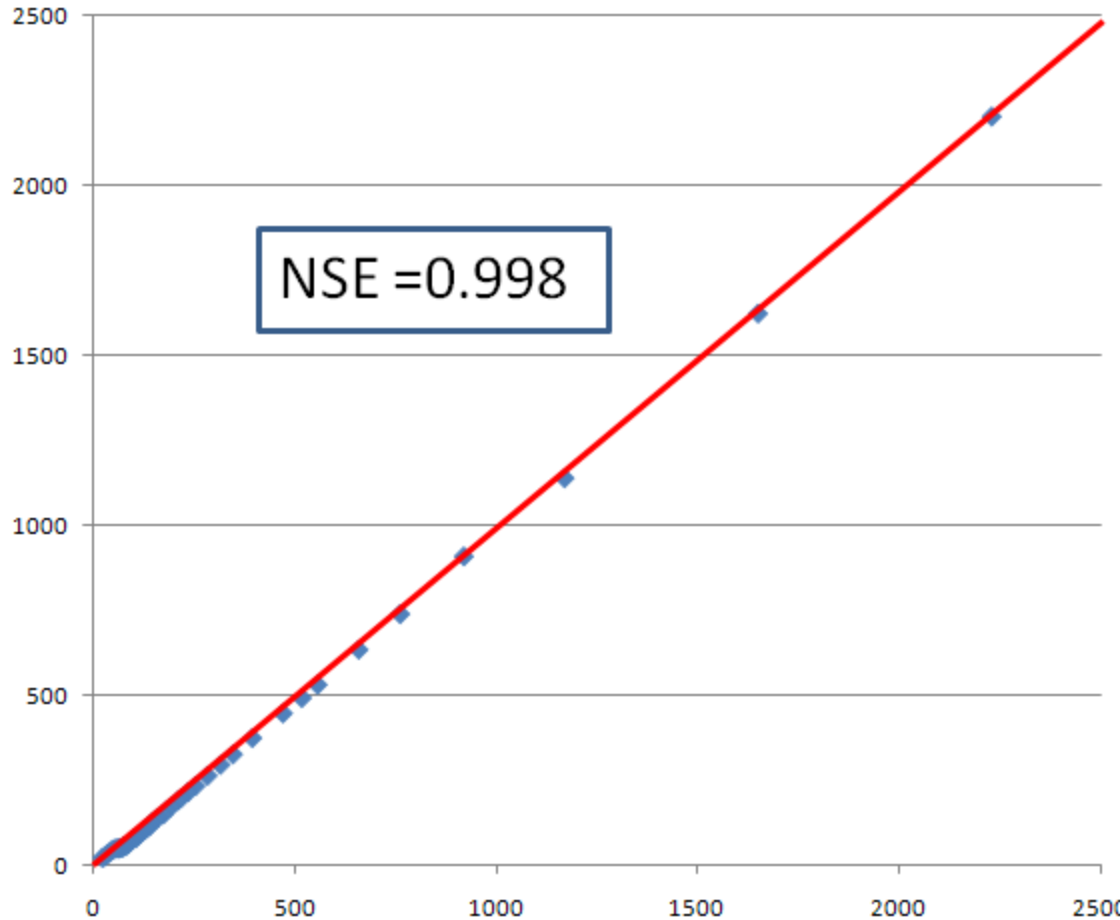
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SWAT model  
Auto-calibration  
Sensitivity analysis

### 1. Introduction

In recent years, application of models has become a valuable tool for the understanding of the natural processes at the watershed scale. Watershed models require a large number of parameters (Sorooshian et al., 1993). The use of such comprehensive models requires a large amount of resources (funds, observed data, time, expertise) which is often unavailable in developing countries. Whilst researchers in the developed countries have used gauged catchments where new models can be validated (Yapo et al., 2005; Yapo et al., 1996), their counterparts in developing countries are forced to apply the models in ungauged catchments (Ndomba et al., 2005; Mulungu and Munishi, 2005).

A comprehensive, complex hydrologic model is often characterized by a multitude of parameters (Eckhardt et al., 2001). Due to spatial variability, measurement errors, and the large number of the required parameters will not



and protection of Europe's aquatic environment. The principal objective of the WFD is to achieve good chemical and ecological status for receiving waters by 2015, and mandates Member States to develop river basin management schemes. This planning mechanism is intended to ensure integrated management of the river environment, providing a decision-making framework for setting environmental objectives. However, the management of water quality from non-point sources would require very expensive monitoring efforts. Mathematical modeling is a necessary step in the implementation

of the WFD. Because of the complexity of the hydrologic processes, hydrologic-based, distributed parameter models and GIS constitute a powerful combination for water quantity and quality assessment [4,5]. There are several reasons that enforce the combination of the aforementioned models with GIS for water resources management, the most important of which are [6]: the automation of data input and output in the pre- and post-processing stage of model development, as well as the ability to develop interactive post-processing tools that provide the opportunity for easier understanding of hydrologic system function; and, the

## Land use changes and hydropower in the Swiss Alpine Rhine basin

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The Swiss Alpine Rhine basin (4108 km<sup>2</sup>) have been modeled with the distributed hydrological catchment model WaSiM-ETH. The model has a resolution of 500 m × 500 m and a temporal resolution of 1 h. The model is used to assess the influence of land use changes on the hydrology in a subcatchment of the Swiss Alps under a scenario of urbanization-afforestation. Furthermore, the influence of reservoirs on the hydrology is investigated. In particular, a significant decrease in low-flow periods in winter. Further, reservoirs functioning as storage for reservoir level data, an attempt has been made to assess the influence of reservoirs on the hydrology. Results show a clear increase in runoff in the land cover change scenarios using WaSiM-ETH. However, its effect is negligible further downstream, especially at the valley bottom. Consequently, the decline in runoff is dependent on the decrease

Urbanization: Afforestation

### Introduction

Economic and demographic growth, increasing population, and consequently, higher electricity demand and the rationalisation and intensification of



□ Introduction

Soil and Water Assessment Tool  
(SWAT)

## □ Introduction

# Calibration SWAT model

Calibration of model  
through adjusting  
input parameter.  
(**Manual calibration**)



## □ Introduction

Calibration SWAT model

Auto Tool



File's

## □ Introduction

# Parameter Solution (Parasol) Method



Finds the **best parameter**  
Based on **Shuffle Complex Evolution(SCE-UA)**

## □ Introduction

Root Mean Square Error (RMSE)

Coefficient of Determination ( $R^2$ )

Index of agreement  $d$

Modified NSE and  $d$

Relative efficiency criteria NSE and  $d$



## □ Objectives of study

- Modification of SWAT Auto-calibration using **different efficiency criteria**.
- Comparison of each SWAT Auto-calibration and finding the **efficiency criteria** which make the **better calibration result**.

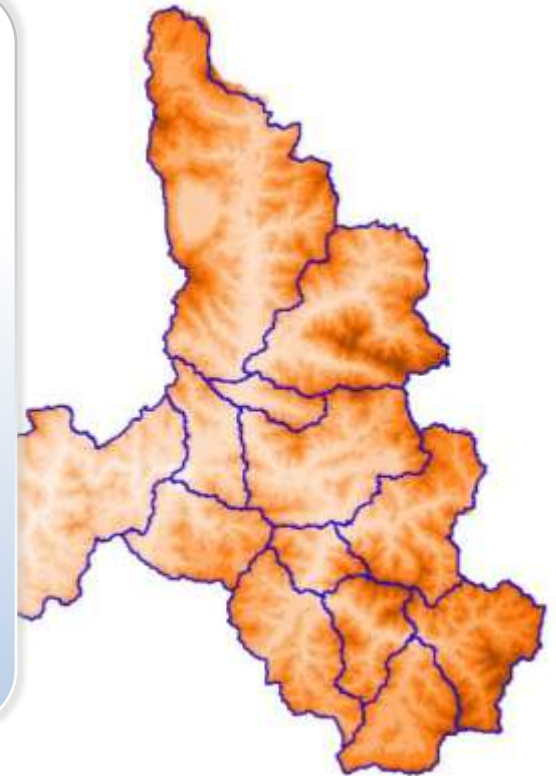
## □ Study Area

Soyanggang dam  
watershed

Area: 2,703 km<sup>2</sup>

Forest : 89.6 %

Agricultural area : 5.3 %



## □ Efficiency criteria

### Nash-Sutcliffe Model Efficiency Coefficient (NSE)

$$NSE = 1 - \frac{\sum_{i=1}^n (O_i - S_i)^2}{\sum_{i=1}^n (O_i - \bar{O})^2}$$

$S_i$  = Simulated data

$O_i$  = Observed data

$\bar{O}$  = The average of observed data

## □ Efficiency criteria

**NSE** with logarithmic values

$$\ln NSE = 1 - \frac{\sum_{i=1}^n (\ln O_i - \ln S_i)^2}{\sum_{i=1}^n (\ln O_i - \ln \bar{O})^2}$$

$S_i$  = Simulated data

$O_i$  = Observed data

$\bar{O}$  = The average of observed data

Using to overcome **oversensitivity** to extreme values

## □ Efficiency criteria

Index of agreement  $d$  (Willmot, 1981)

$$d = 1 - \frac{\sum_{i=1}^n (O_i - S_i)^2}{\sum_{i=1}^n (|S_i - \bar{O}| + |O_i - \bar{O}|)^2}$$

$S_i$  = Simulated data

$O_i$  = Observed data

$\bar{O}$  = The average of observed data

Using to overcome **insensitivity** of NSE and  $R^2$

## □ Efficiency criteria

Modified forms of **NSE** and ***d***

$$NSE_m = 1 - \frac{\sum_{i=1}^n |O_i - S_i|}{\sum_{i=1}^n |O_i - \bar{O}|}$$

$$d_m = 1 - \frac{\sum_{i=1}^n |O_i - S_i|}{\sum_{i=1}^n (|S_i - \bar{O}| + |O_i - \bar{O}|)}$$

Same purpose logarithmic NSE and Index of *d*

## □ Efficiency criteria

Relative efficiency criteria **NSE** and **d**

$$NSE_{rel} = 1 - \frac{\sum_{i=1}^n \left( \frac{O_i - S_i}{O_i} \right)^2}{\sum_{i=1}^n \left( \frac{O_i - \bar{O}}{\bar{O}} \right)^2}$$

$$d_{rel} = 1 - \frac{\sum_{i=1}^n \left( \frac{O_i - S_i}{O_i} \right)^2}{\sum_{i=1}^n \left( |S_i - \bar{O}| + |O_i - \bar{O}| \right)^2}$$

More sensitive in particular during low flow conditions

## □ Methods

The **objective function** of current SWAT Auto-calibration



Sum of the **squares** of the residuals(**SSQ**)

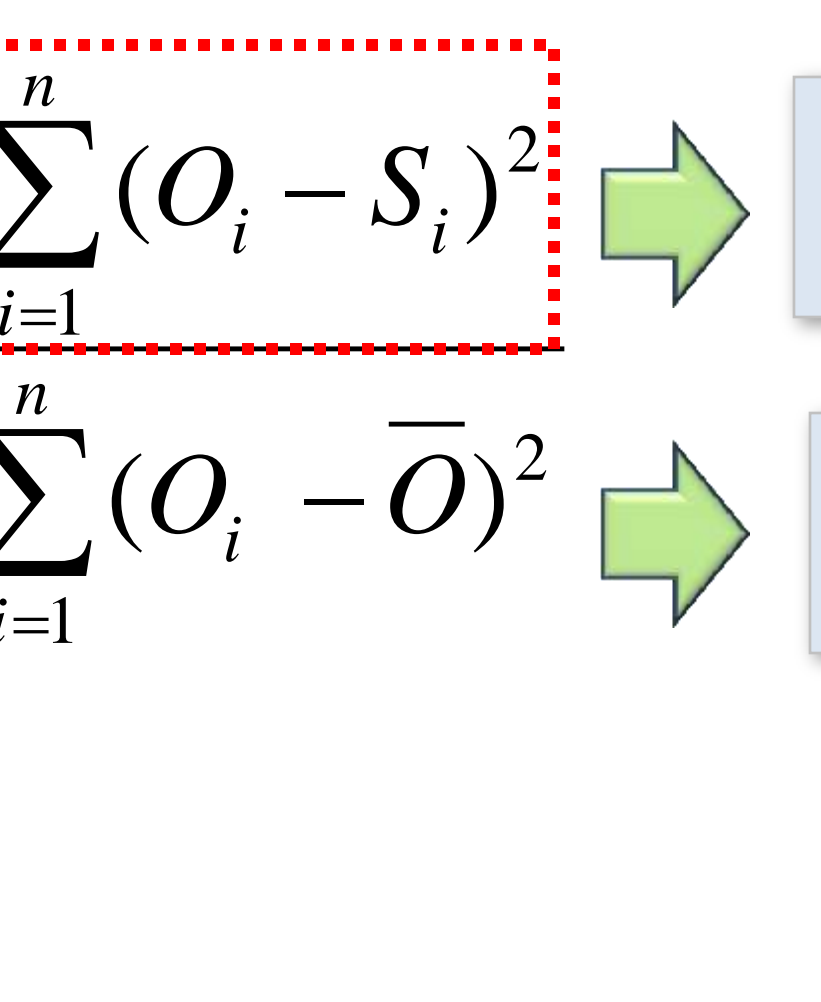


## □ Methods

$$NSE = 1 - \frac{\sum_{i=1}^n (O_i - S_i)^2}{\sum_{i=1}^n (O_i - \bar{O})^2}$$

SSQ

Fixed



## □ Methods

**NSE** with **logarithmic** values

$$\ln NSE = 1 - \frac{\sum_{i=1}^n (\ln O_i - \ln S_i)^2}{\sum_{i=1}^n (\ln O_i - \ln \bar{O})^2}$$

Index of agreement **d**

$$d = 1 - \frac{\sum_{i=1}^n (O_i - S_i)^2}{\sum_{i=1}^n (|S_i - \bar{O}| + |O_i - \bar{O}|)^2}$$

Modified forms of **NSE**

$$NSE_m = 1 - \frac{\sum_{i=1}^n |O_i - S_i|}{\sum_{i=1}^n |O_i - \bar{O}|}$$

Modified forms of **d**

$$d_m = 1 - \frac{\sum_{i=1}^n |O_i - S_i|}{\sum_{i=1}^n (|S_i - \bar{O}| + |O_i - \bar{O}|)}$$

## □ Methods

Relative efficiency criteria **NSE**

$$NSE_{rel} = 1 - \frac{\sum_{i=1}^n \left( \frac{O_i - S_i}{O_i} \right)^2}{\sum_{i=1}^n \left( \frac{O_i - \bar{O}}{\bar{O}} \right)^2}$$

Relative efficiency criteria **d**

$$d_{rel} = 1 - \frac{\sum_{i=1}^n \left( \frac{O_i - S_i}{O_i} \right)^2}{\sum_{i=1}^n \left( \frac{|S_i - \bar{O}| + |O_i - \bar{O}|}{\bar{O}} \right)^2}$$

Modified SWAT auto-calibration can consider various efficiency criteria

## □ Methods

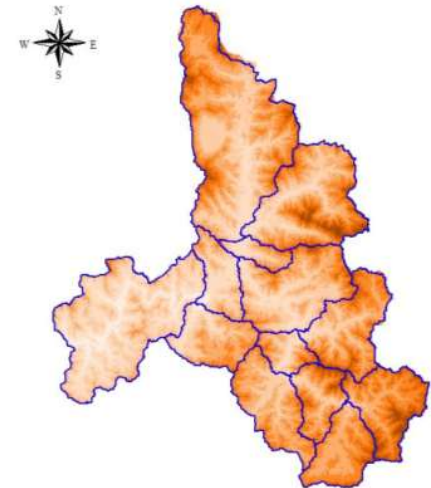
### Modified SWAT Auto-calibration

**NSE** with **logarithmic** values

Index of agreement ***d***

Modified **NSE** and ***d***

Relative efficiency criteria **NSE** and ***d***

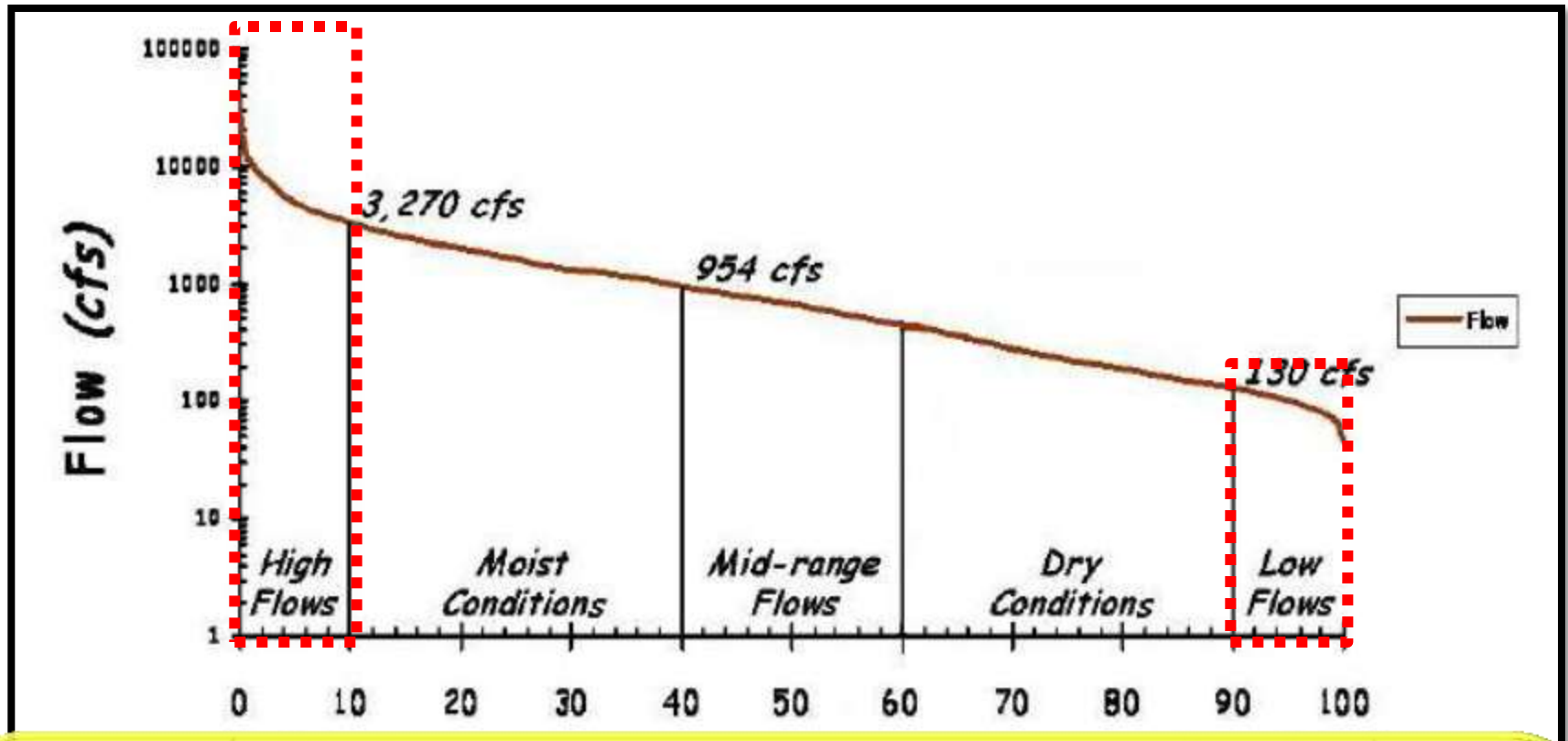


Daily Simulation in 2006

# □ Methods

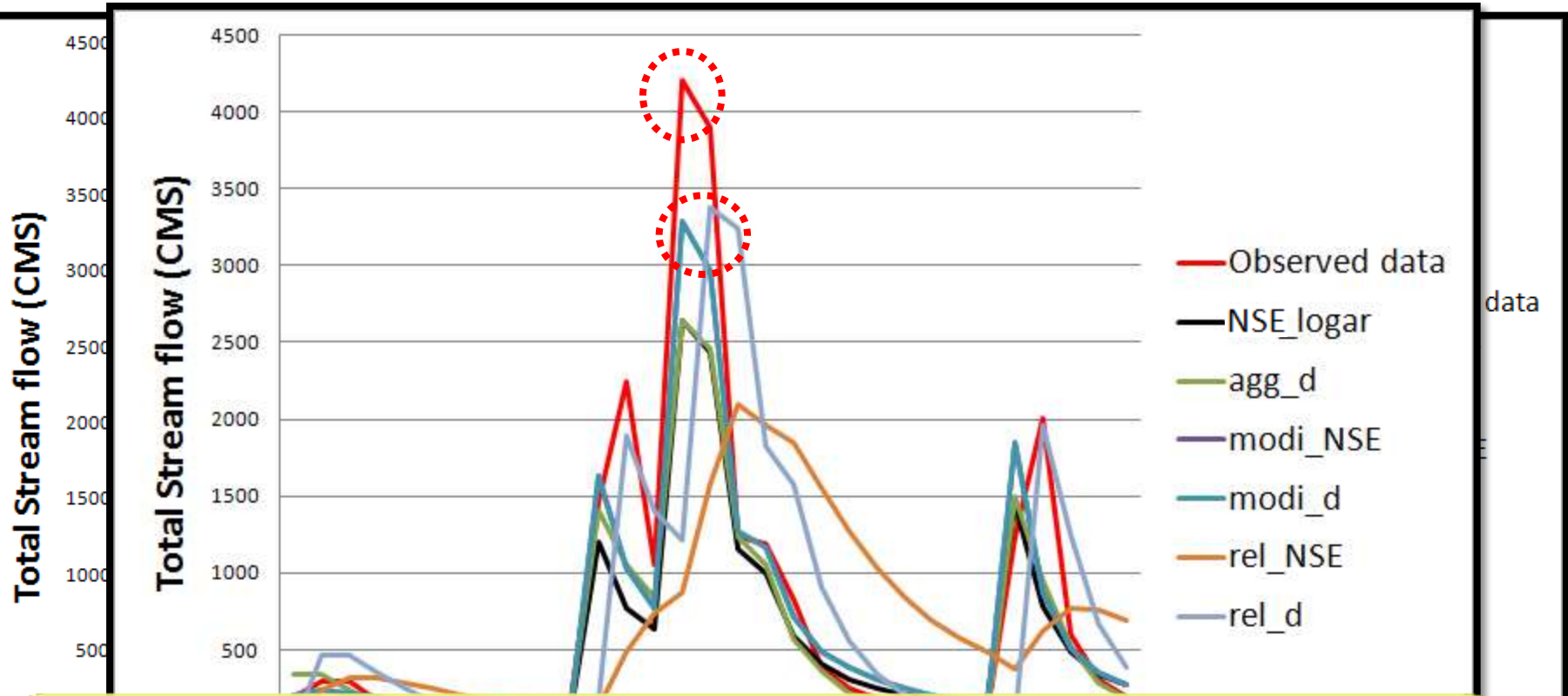
Parameter	Description
ALPHA_BF	Baseflow alpha factor
BIOMIX	Biological mixing efficiency
BLAI	Maximum potential leaf area index
CANMX	Maximum canopy storage
CH_K2	Effective hydraulic conductivity in main channel alluvium
CH_N2	Mannings' "n" value for the main channel
CN2	SCS runoff curve number for moisture condition II
EPCO	Plant evaporation compensation factor
ESCO	Soil evaporation compensation factor
GW_DELAY	Groundwater delay
GW_REVAP	Groundwater "revap" coefficient
GWQMN	Threshold depth of water in the shallow aquifer required for return flow to occur
REVAPMN	Threshold depth of water in the shallow aquifer for "revap" to occur (mm)
SFTMP	Snow melt base temperature (° C)
SLOPE	Increase the lateral flow
SLSUBBSN	Average slope length
SMFMN	Minimum melt rate for snow (mm/° C/day)
SMFMX	Maximum melt rate for snow (mm/° C/day)
SMTMP	Snow melt base temperature (° C)
SOL_AIB	Moist soil albedo
SOL_AWC	Available water capacity of the soil layer
SOL_K	Saturated hydraulic conductivity (mm/hr)
SOL_Z	Soil depth (%)
SURLAG	Surface runoff lag time
TIMP	Snow pack temperature lag factor
TLAPS	Temperature laps rate (° C/km)

## □ Methods



Each SWAT auto-calibration was compared in total stream flow, high and low flow conditions

## □ Results



Each auto-calibration was generated among the over 10,000 simulations

## □ Results

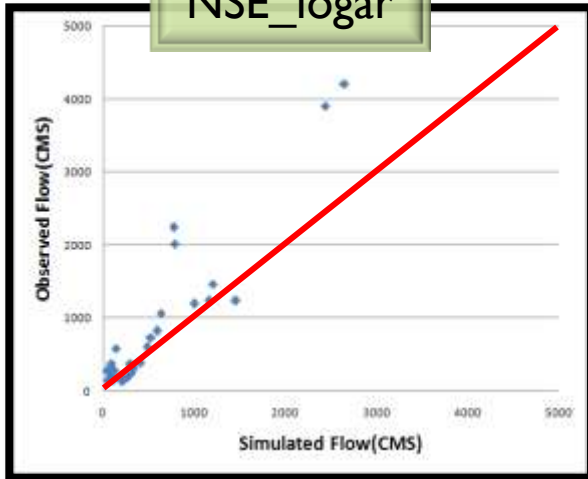
Comparison of Auto-calibration for **high flow** condition(top 10% )

Efficiency criteria Type of objective function	NSE	NSE_logar	Agg_d	NSE <sub>m</sub>	$d_m$	NSE <sub>rel</sub>	$d_{rel}$
NSE_logar	<b>0.72</b>	<b>0.5</b>	<b>0.9</b>	<b>0.57</b>	<b>0.76</b>	<b>0.87</b>	<b>0.95</b>
Agg_d	<b>0.77</b>	<b>0.87</b>	<b>0.91</b>	<b>0.66</b>	<b>0.81</b>	<b>0.90</b>	<b>0.96</b>
NSE <sub>m</sub>	<b>0.84</b>	<b>0.85</b>	<b>0.95</b>	<b>0.68</b>	<b>0.83</b>	<b>0.91</b>	<b>0.97</b>
$d_m$	<b>0.84</b>	<b>0.85</b>	<b>0.95</b>	<b>0.68</b>	<b>0.83</b>	<b>0.91</b>	<b>0.97</b>
NSE <sub>rel</sub>	<b>0.40</b>	<b>0.37</b>	<b>0.71</b>	<b>0.28</b>	<b>0.56</b>	<b>-0.18</b>	<b>0.44</b>
$d_{rel}$	<b>0.86</b>	<b>0.79</b>	<b>0.96</b>	<b>0.63</b>	<b>0.80</b>	<b>0.68</b>	<b>0.90</b>

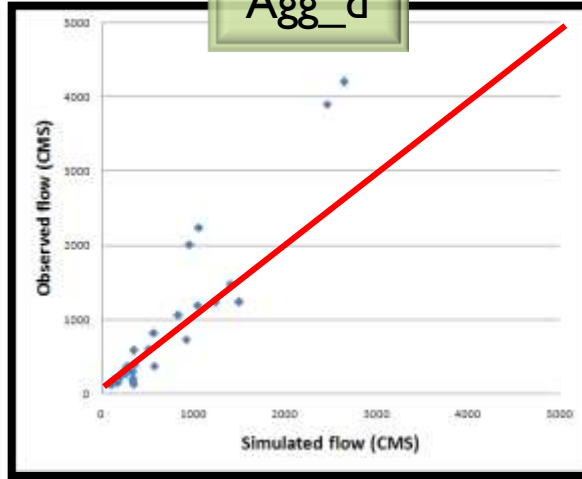


# Results

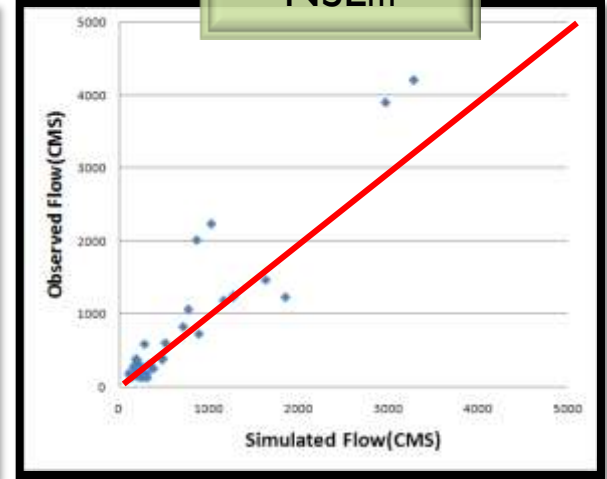
NSE\_logar



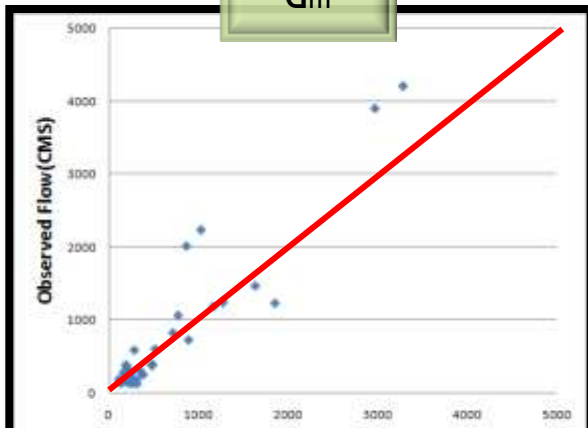
Agg\_d



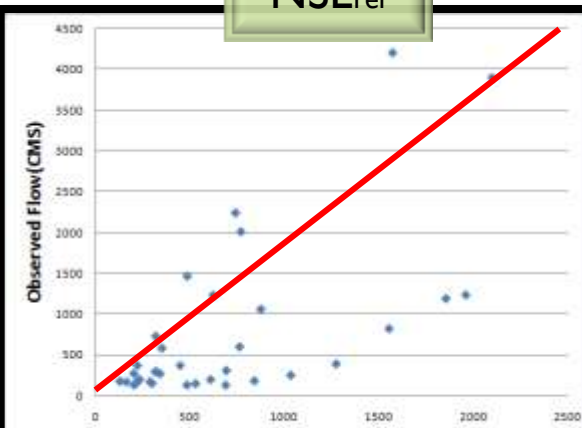
NSEm



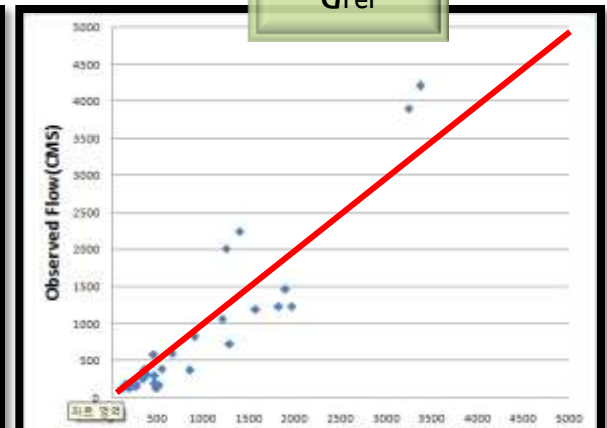
d<sub>m</sub>



NSE<sub>rel</sub>



d<sub>rel</sub>



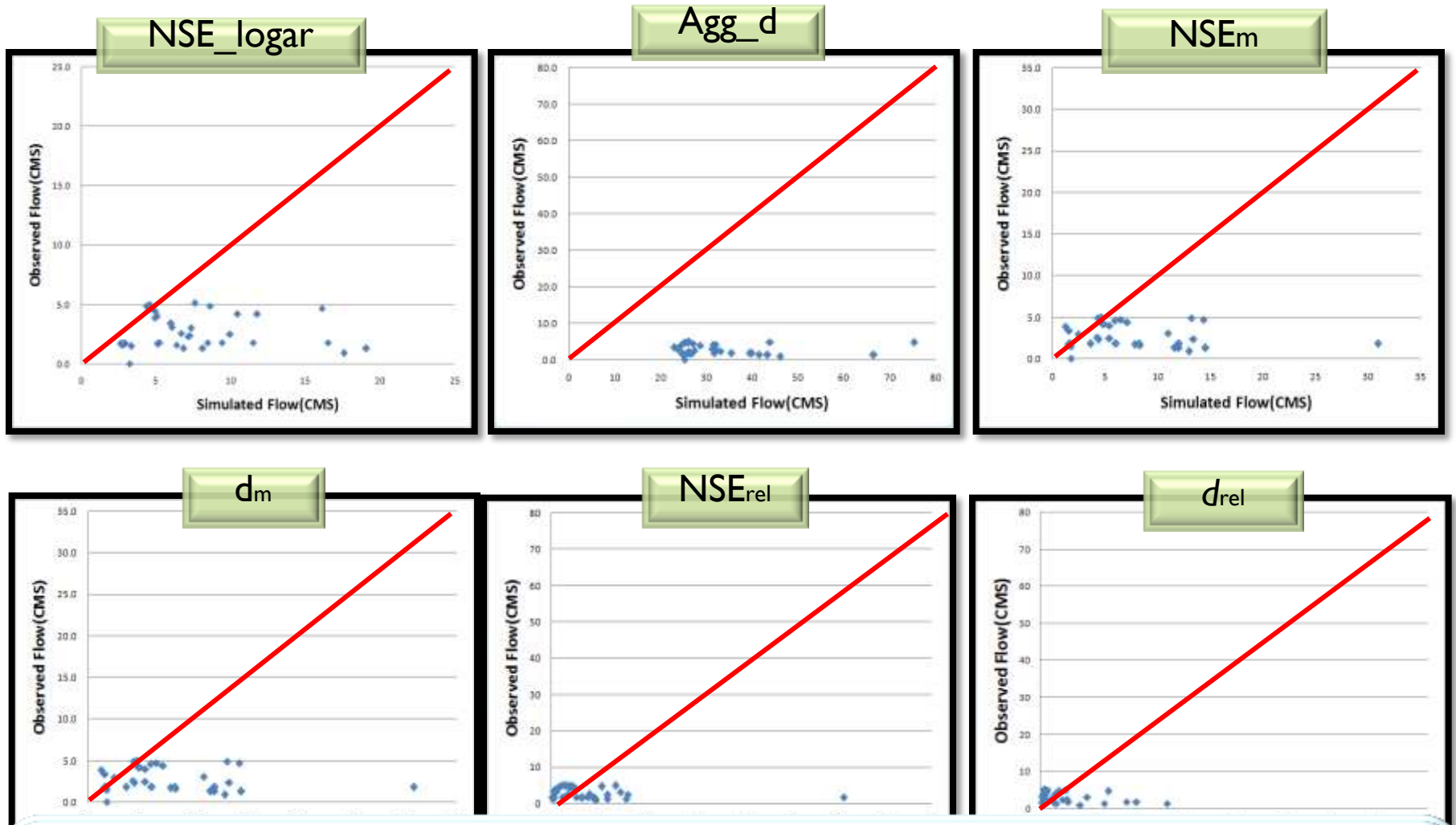
Reasonable result for high flow condition

## □ Results

### Comparison of Auto-calibration for **low flow** condition(bottom 10%)

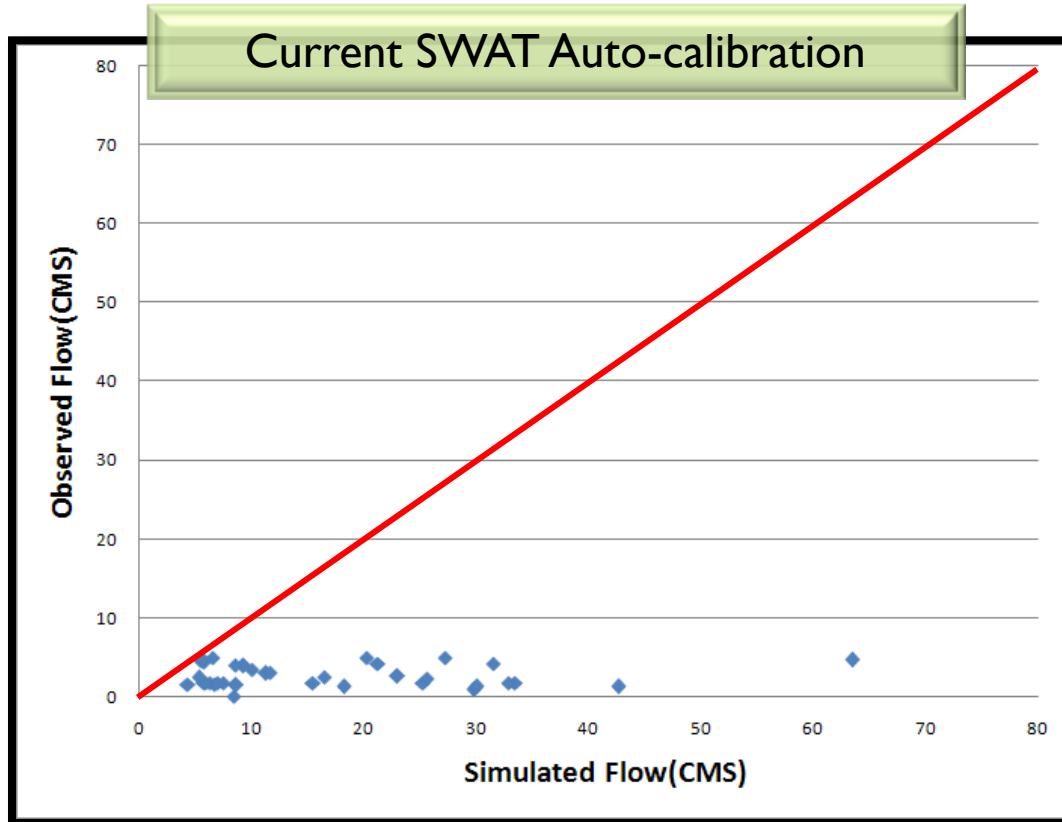
Efficiency criteria Type of objective function	NSE	NSE_logar	Agg_d	NSE <sub>m</sub>	$d_m$	NSE <sub>rel</sub>	$d_{rel}$
NSE_logar	<b>-20.59</b>	<b>-0.20</b>	<b>0.35</b>	<b>-2.80</b>	<b>0.20</b>	<b>-88.08</b>	<b>-2.14</b>
Agg_d	<b>-535.70</b>	<b>-1.09</b>	<b>0.07</b>	<b>-23.36</b>	<b>0.04</b>	<b>-1426.74</b>	<b>-1.29</b>
NSE <sub>m</sub>	<b>-29.49</b>	<b>-0.15</b>	<b>0.16</b>	<b>-3.00</b>	<b>0.22</b>	<b>-95.33</b>	<b>-1.46</b>
$d_m$	<b>-29.49</b>	<b>-0.15</b>	<b>0.16</b>	<b>-3.00</b>	<b>0.22</b>	<b>-95.33</b>	<b>-1.46</b>
NSE <sub>rel</sub>	<b>-70.55</b>	<b>-7.16</b>	<b>0.11</b>	<b>-3.72</b>	<b>0.16</b>	<b>-2254.60</b>	<b>-1.38</b>
$d_{rel}$	<b>-24.02</b>	<b>-6.70</b>	<b>0.24</b>	<b>-2.32</b>	<b>0.20</b>	<b>-1056.67</b>	<b>-2.00</b>

# Results



**Unreasonable** calibration result for **low flow condition**

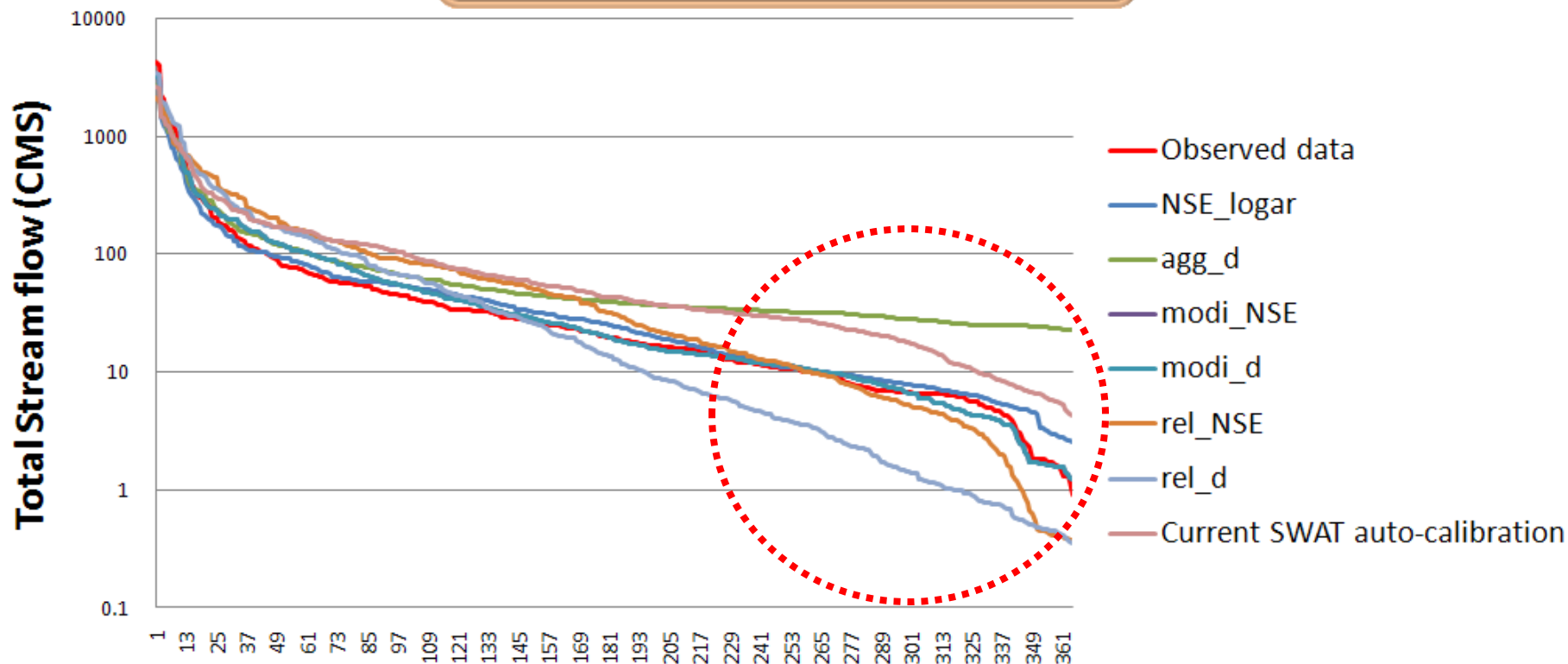
## □ Results



**Unreasonable** calibration result for **low flow condition**

## □ Results

Flow Duration Curve



## □ Conclusion

- In this study, SWAT Auto-calibration was modified by **different efficiency criteria**.
- As a result of this study, Auto-calibrations modified by modi\_NSE, modi\_d and rel\_d show the better calibration result **for high flow** conditions.

## □ Conclusion

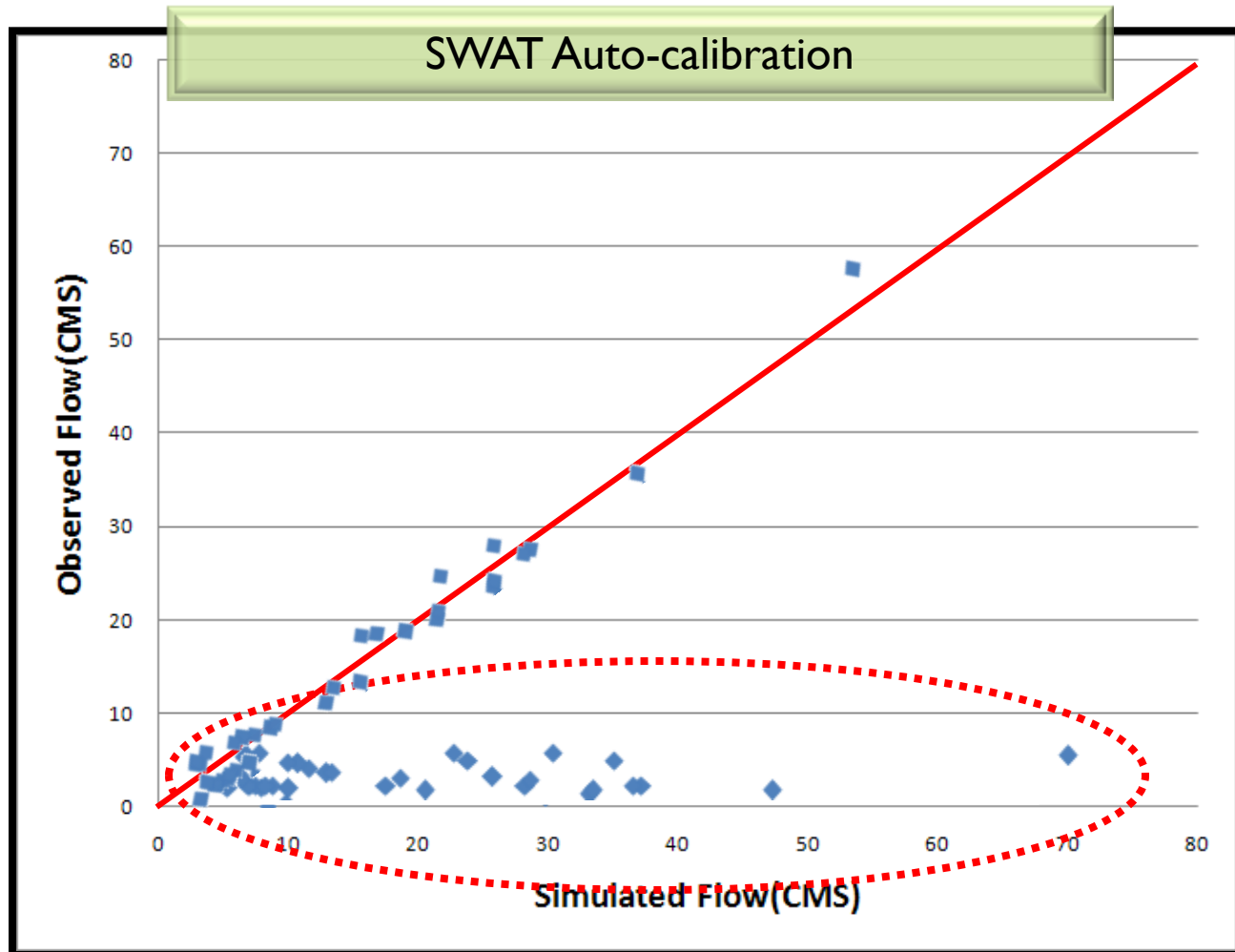
- In low flow conditions, the results of all auto-calibrations are **unacceptable**.
- SWAT Auto-calibration should be improved and modified to make the better simulation for low flow conditions.

## □ Conclusion

- For better calibration and validation of hydrological modeling, combination and comparison of different efficiency criteria is needed.
- The result of this study can be used to improve the accuracy of SWAT Auto-calibration for various flow conditions.



## □ Future study



# GIS Environment System Lab.

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